RARE-EARTH MAGNET AND METHOD OF MANUFACTURING SAME

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Inventor: MORI MASAMI; TANAKA MICHI; SAKAMOTO

TAKESHI; MIWA MASASHI

Applicant: TDK CORP

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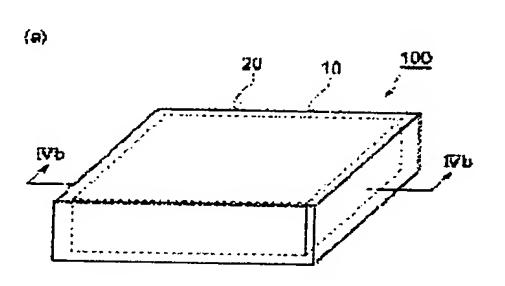
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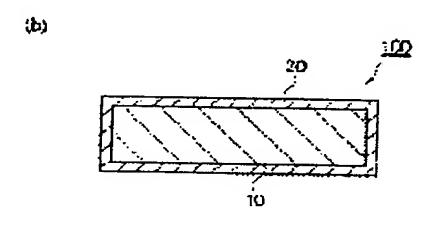
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Abstract of JP2005286031

PROBLEM TO BE SOLVED: To provide a method by which a rare-earth magnet that has sufficiently excellent magnetic characteristics and, in addition, is sufficiently excellent in corrosion resistance can be manufactured, and to provide the rare-earth magnet. SOLUTION: The method of manufacturing the rare-earth magnet includes a noncrystallizing process of preparing a polycrystalline elemental magnet body 10 containing a rare-earth element and noncrystallizing the surface layer of the magnet body 10. COPYRIGHT: (C)2006, JPO&NCIPI





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CLAIMS

[Claim(s)]

[Claim 1]

The manufacture approach of a rare earth magnet equipped with an amorphous chemically-modified [which prepares the magnet element assembly of polycrystal, including rare earth elements, and makes the surface of said magnet element assembly amorphous] degree.

[Claim 2]

The manufacture approach of the rare earth magnet according to claim 1 which gives an impact to the surface of said magnet element assembly, and makes the surface of said magnet element assembly amorphous to an amorphous chemically-modified [said] degree.

[Claim 3]
The manufacture approach of a rare earth magnet according to claim 2 of making a particle group colliding with the surface of said magnet element assembly to an amorphous chemically-modified [said] degree.

[Claim 4]

A rare earth magnet given in any of claims 1-3 which make amorphous the part from the front face of said magnet element assembly to a depth of 0.1-20 micrometers to an amorphous chemically-modified [said] degree they are.

[Claim 5]

The manufacture approach of a rare earth magnet given in any of claims 1-4 further equipped with the chemical conversion process which carries out chemical conversion of the surface of said layer made amorphous, and forms a passivation layer after an amorphous chemically-modified [said] degree they are.

[Claim 6]

The manufacture approach of a rare earth magnet according to claim 5 of contacting at least one of a nitric acid, a zinc phosphate water solution, the oxygen plasma, and ozone on the surface of said amorphous layer at said chemical conversion process.

[Claim 7]

Rare earth elements are included and it is the magnet element assembly of polycrystal,

It has the amorphous layer formed on said magnet element assembly,

Said amorphous layer is a rare earth magnet containing all the elements that constitute said magnet element assembly.

[Claim 8]

The presentation ratio of the element which constitutes said magnet element assembly in said magnet element assembly and said amorphous layer is the same rare earth magnet according to claim 7. [Claim 9]

Rare earth elements are included and it is the magnet element assembly of polycrystal,

It has the amorphous layer formed on said magnet element assembly,

Said amorphous layer is a rare earth magnet which makes said magnet element assembly amorphous.

[Claim 10]

Said amorphous layer is a rare earth magnet given in any of claims 7-9 which have the thickness of 0.1-20 micrometers they are.

[Claim 11]

A rare earth magnet given in any 1 term of claims 7-10 further equipped with the passivation layer which carried out chemical conversion of said amorphous layer, and passivated it on said amorphous layer.

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[Field of the Invention]

[0001]

This invention relates to the manufacture approach of a rare earth magnet, and a rare earth magnet. [Background of the Invention]

[0002]

Conventionally, the rare earth magnet containing rare earth elements, such as Nd, is known as a permanent magnet in which a high energy product is shown. Since this kind of rare earth magnet contains the rare earth elements which oxidize comparatively easily as a principal component, that corrosion resistance is comparatively low. Therefore, it originated in this and technical problems, like that the engine performance as a magnet deteriorates at the time of manufacture and use or the manufactured magnetic dependability is comparatively low occurred. And the proposal which forms a protective layer in the front face of a magnet element assembly for the purpose of improving the corrosion resistance of such a rare earth magnet is made.

[0003]

For example, by the patent reference 1, in the argon, the nitrogen, or the low-vacuum ambient atmosphere where oxygen tension is 10-6 - 1Torr, scaling processing of 10 minutes - 10 hours is performed to a magnet element assembly with the heat treatment temperature of 200-1100 degrees C, and the approach of using the surface of a magnet element assembly as the low-grade oxide film of the magnet element assembly ingredient as a protective layer is proposed.

[0004]

Moreover, the approach of forming the protective layer made of about 5-25-micrometer resin in the front face of a magnet element assembly is indicated by the patent reference 2.

[Patent reference 1] JP,2002-57052,A

[Patent reference 2] JP,60-63901,A

[Description of the Invention]

[Problem(s) to be Solved by the Invention]

[0005]

However, when this invention persons inquired in the detail, it became clear that there were the following technical problems in the rare earth magnet which has the conventional protective layer. [0006]

Namely, since a magnet element assembly is put to an elevated temperature at the time of manufacture, as for the rare earth magnet which used the surface of a magnet element assembly ingredient as the oxide film as a protective layer by heat treatment, magnetic properties, such as magnetic flux in a magnet element assembly, deteriorate in many cases.

[0007]

On the other hand, between a magnet element assembly and a protective layer, since the difference of physical properties, such as coefficient of thermal expansion, is large, the rare earth magnet in which protective layers, such as resin, were formed on the front face of a magnet element assembly does not have the enough adhesion of a protective layer and a magnet element assembly, a crack arises in a protective layer or a protective layer becomes easy to separate. For this reason, corrosion resistance becomes inadequate in many cases.

[8000]

It aims at offering the manufacture approach of a rare earth magnet and rare earth magnet in which this invention is made in view of the above-mentioned situation, and have the magnetic properties which were fully excellent, and corrosion resistance was fully excellent.

[Means for Solving the Problem]

[0009]

The manufacture approach of the rare earth magnet concerning this invention prepares the magnet element assembly of polycrystal, including rare earth elements, and is equipped with an amorphous chemically-modified [which makes the surface of this magnet element assembly amorphous] degree.

[0010]

Here, the solid-state structure where polycrystal comes to gather in many single crystal grains which the atom arranged regularly is said, and, as for an amorphous substance, an atom says the solid-state structure arranged irregularly.

[0011]

Generally, a rare earth magnet takes the polycrystal structure which contains at least the crystalline main phase containing rare earth elements, and the grain boundary phase containing the rare earth elements by which it is placed between the main interphases. And since many lattice defects are included in a grain boundary phase, it is very easy to diffuse corrosion components, such as oxygen, to this grain boundary phase. Moreover, rare earth elements are elements which tend to be originally corroded by corrosion components, such as oxygen. Therefore, if the part of polycrystal is exposed to the surface of a rare earth magnet, corrosion will progress along with this grain boundary phase, and the crystal grain of the main phase will be omitted.

[0012]

However, according to this invention, the rare earth magnet which allotted the wrap amorphous layer is formed in this magnet element assembly on the magnet element assembly of polycrystal by making amorphous the surface of the magnet element assembly of such polycrystal. There is almost no regular array structure of an atom like polycrystal in this amorphous layer, and the atom has arranged irregularly. Therefore, the part which the corrosion matter tends to diffuse alternatively like the grain boundary phase in polycrystal cannot exist in an amorphous layer easily, and it is hard to diffuse corrosion components, such as oxygen, in this amorphous layer. Thereby, this amorphous layer functions as a protective layer which protects the magnet element assembly of polycrystal from corrosion components, such as oxygen.

[0013]

Furthermore, in order that this amorphous layer may make a magnet element assembly amorphous, as for a magnet element assembly and an amorphous layer, physical properties, such as coefficient of thermal expansion, will become mutual very near. Therefore, the adhesion of an amorphous layer and a magnet element assembly becomes good, a crack occurs in an amorphous layer or an amorphous layer stops being able to separate from a magnet element assembly easily. By this, a rare earth magnet will demonstrate sufficient corrosion resistance. Moreover, since generating or peeling of the crack of an amorphous layer cannot take place easily, generating of contamination components, such as particle from a rare earth magnet, decreases extremely, and is desirable. [0014]

In addition, since amorphous-ization of such a magnet element assembly can be performed giving an impact to the surface of a magnet element assembly, by irradiating an atomic beam, a molecule beam, an ion beam, an electron ray, etc. at the surface of a magnet element assembly, etc., it is not necessary to expose a magnet element assembly to an elevated temperature. Therefore, magnetic properties, such as magnetic flux of a magnet element assembly, hardly deteriorate at the time of manufacture, but the magnetic properties which were fully excellent can be demonstrated. [0015]

Here, to an amorphous chemically-modified degree, it is desirable to give an impact to the surface of a magnet element assembly and to make the surface of a magnet element assembly amorphous. [0016]

According to this,-izing of the surface of a magnet element assembly can be carried out

[amorphous] easily. Moreover, a precise amorphous layer can be formed as compared with irradiating an atomic beam, a molecule beam, an ion beam, an electron ray, etc., and making them amorphous, and the corrosion of the amorphous layer itself can fully be controlled.
[0017]

By getting a mechanical impact, for example as a reason which a magnet element assembly makes amorphous by giving an impact here, compressive stress and shearing stress join the surface of a magnet element assembly, plastic deformation happens, and atomic regular structure is confused and is considered to make it amorphous by this.

[0018]

Here, more specifically, it is desirable to give an impact to the surface of a magnet element assembly using the so-called blasting or the approach called shot peening of making a particle group collide with the surface of a magnet element assembly.

[0019]

According to this, it is easy to repeat and give a moderate impact to the surface of a magnet element assembly. If a spherical particle group is used especially, since an impact can be given fully controlling wear of the surface of a magnet element assembly etc., amorphous-ization can be performed very efficiently.

[0020]

As an ingredient of a particle, the ceramic ingredient of SiO2, SiC, and aluminum2O3 grade is mentioned, for example. Moreover, metallic materials, such as the Steel shot, can also be used as an ingredient of a particle.

[0021]

Moreover, to an amorphous chemically-modified degree, when the part from the front face of a magnet element assembly to a depth of 0.1-20 micrometers is made amorphous, it is desirable. Even if the depth from a front face makes only a less than 0.2-micrometer part amorphous, there is an inclination which corrosion resistance stops being able to demonstrate sufficiently easily. Even if it makes amorphous even the part of the depth of 20-micrometer ** from a front face, corrosion resistance does not improve any more, but the cost which amorphous-ization takes becomes high and it becomes on the other hand, less efficient [tend]. [0022]

By the way, although the magnet element assembly of a rare earth magnet can fully be protected by the amorphous layer which carried out in this way and was formed, depending on the presentation of an amorphous layer, the amorphous layer itself may corrode a little.

[0023]

Then, it is desirable to have further the chemical conversion process which carries out chemical conversion of the surface of an amorphous layer, and forms a passivation layer after an amorphous chemically-modified degree.

[0024]

In this case, by the passivation layer, the corrosion of the amorphous layer itself is also reduced further and the further corrosion resistance improvement in a rare earth magnet of it is attained. [0025]

Specifically as chemical conversion, contacting at least one of a nitric acid, a zinc phosphate water solution, the oxygen plasma, and ozone on the surface of an amorphous layer is mentioned. [0026]

The rare earth magnet of this invention is equipped with a wrap amorphous layer for the front face of the magnet element assembly of polycrystal, and this magnet element assembly, including rare earth elements, and an amorphous layer contains all the elements that constitute a magnet element assembly.

[0027]

According to this invention, a grain boundary phase hardly exists in an amorphous layer, but this amorphous layer functions as a protective layer which protects a magnet element assembly from corrosion components, such as oxygen, as mentioned above. Moreover, this amorphous layer contains all the configuration elements of a magnet element assembly. Therefore, the physical properties of a magnet element assembly and an amorphous layer will become near mutually, the

adhesion of an amorphous layer and a magnet element assembly becomes good, and sufficient corrosion resistance is demonstrated.

[0028]

Moreover, the rare earth magnet of such a configuration can be manufactured easily, without exposing a magnet element assembly to an elevated temperature by the above-mentioned manufacture approach. Therefore, the rare earth magnet of magnetic properties high enough is realizable.

[0029]

Here, in a magnet element assembly and an amorphous layer, the same thing of the presentation ratio of the element which constitutes a magnet element assembly is desirable. In this case, since the physical properties of an amorphous layer and a magnet element assembly become nearer, the adhesion of a magnet element assembly and an amorphous layer can be improved more. Here, such an amorphous layer can be formed by giving an impact to the surface of a magnet element assembly, for example.

[0030]

If the rare earth magnet concerning this invention is expressed from another viewpoint, the rare earth magnet concerning this invention will be equipped with the amorphous layer formed on the magnet element assembly of polycrystal, and the magnet element assembly, including rare earth elements, and an amorphous layer will make this magnet element assembly amorphous.

[0031]

Such a rare earth magnet does so the same operation effectiveness as an above-mentioned rare earth magnet.

[0032]

As for an amorphous layer, also in which an above-mentioned rare earth magnet, it is desirable to have the thickness of 0.1-20 micrometers. When the thickness of an amorphous layer is thinner than 0.1 micrometers, there is an inclination sufficiently to be hard coming to demonstrate corrosion resistance. Even if it forms an amorphous layer thicker than 20 micrometers, corrosion resistance does not improve any more, but the cost which formation of an amorphous layer takes becomes high, and it becomes on the other hand, less efficient [tend].

It is desirable to have further the passivation layer which comes to carry out chemical conversion of this amorphous layer on an amorphous layer here. In this case, by the passivation layer, the corrosion of the amorphous layer itself is also reduced further and the further corrosion resistance improvement in a rare earth magnet of it is attained.

[0034]

As a magnet element assembly in such a rare earth magnet, rare earth elements, iron, and the magnet element assembly containing boron can be used, for example. This magnet element assembly can obtain the rare earth magnet which has high magnetic properties and has high corrosion resistance by using this kind of magnet element assembly for the rare earth magnet concerning this invention, although magnetic properties are known for a very high thing.

[Effect of the Invention]

[0035]

According to this invention, the manufacture approach of a rare earth magnet and rare earth magnet which have the magnetic properties and corrosion resistance which were fully excellent can be offered.

[Best Mode of Carrying Out the Invention]

[0036]

Hereafter, referring to a drawing if needed, about the suitable operation gestalt of this invention, especially physical relationship, such as explanation **** and four directions, shall be based on the physical relationship shown in a drawing at a detail, unless it refuses. Furthermore, the dimension ratio of a drawing is not restricted to the ratio of illustration.

[0037]

(The first operation gestalt)

The manufacture approach of a rare earth magnet 100 and rare earth magnet 100 which are first

applied to the first operation gestalt of this invention are explained. [0038]

(Preparation of a magnet element assembly)

First, as shown in <u>drawing 1</u> (a), the magnet element assembly 10 of polycrystal is prepared, including rare earth elements.

[0039]

The magnet element assembly 10 is a magnet containing rare earth elements R, iron (Fe), and boron (B). Rare earth elements R show one or more sorts of rare earth elements, and show one or more sorts of elements chosen from the group which specifically consists of the scandium (Sc), yttrium (Y), and lanthanoids belonging to three groups of the long period mold periodic table. Here, a lanthanoids points out a lanthanum (La), a cerium (Ce), a praseodymium (Pr), neodymium (Nd), samarium (Sm), a europium (Eu), a gadolinium (Gd), a terbium (Tb), a dysprosium (Dy), a holmium (Ho), an erbium (Er), a thulium (Tm), an ytterbium (Yb), and a lutetium (Lu).

When one or more sorts of elements are included among Nd, Pr, Ho, and Tb as rare earth elements R among what was mentioned above, it is desirable, and it is still more desirable although one or more sorts of elements are included among La, Sm, Ce, Gd, Er, Eu, Tm, Yb, and Y. [0041]

The content rate of the rare earth elements R in the magnet element assembly 10 is desirable in it being eight to 40 atom % to the amount of all the atoms that constitute the magnet element assembly 10. Under by 8 atom %, since the crystal structure serves as a cubic organization of the same structure as alpha-iron, the content rate of rare earth elements R is in the inclination for the rare earth magnet 100 which has high coercive force (iHc) not to be obtained. moreover -- if the content rate of rare earth elements R exceeds 40 atom % -- R -- a rich nonmagnetic phase increases and it is in the inclination for the residual magnetic flux density (Br) of a rare earth magnet 100 to fall. [0042]

The content rate of Fe in the magnet element assembly 10 is desirable in it being 42 to 90 atom % to the amount of all the atoms that constitute the magnet element assembly 10. It is in the inclination for Br of a rare earth magnet 100 to fall that the content rate of Fe is under 42 atom %, and when 90 atom % is exceeded, it is in the inclination for iHc of a rare earth magnet 100 to fall. [0043]

The content rate of B in the magnet element assembly 10 is desirable in it being two to 28 atom % to the amount of all the atoms that constitute the magnet element assembly 10. since the crystal structure becomes that the content rate of B is under 2 atom % with a rhombohedron organization, if it is in the inclination which becomes inadequate [iHc of a rare earth magnet 100] and 28 atom % is exceeded -- B -- since a rich nonmagnetic phase increases, it is in the inclination for Br of a rare earth magnet 100 to fall.

[0044]

Moreover, cobalt (Co) may permute a part of Fe, and the magnet element assembly 10 may be constituted. It is in the inclination for the temperature characteristic to be improvable, by making it such a configuration, without spoiling the magnetic properties of a rare earth magnet 100. In this case, the content rate of Fe and Co after a permutation is desirable in Co/(Fe+Co) being 0.5 or less on atomic criteria. When there are more amounts of permutations of Co than this, it is in the inclination for the magnetic properties of a rare earth magnet 100 to fall.

[0045]

Furthermore, one or more sorts of elements chosen from the group which consists of (Carbon C) Lynn (P), sulfur (S), and copper (Cu) may permute a part of B, and the magnet element assembly 10 may be constituted. By making it this configuration, the productivity of a rare earth magnet 100 improves and it is in the inclination which can reduce the production cost. In this case, the content of these [C, P, and S] and/, or Cu is desirable in it being below 4 atom % to the amount of all the atoms that constitute the magnet element assembly 10. When there are more contents of C, P, S and/, or Cu than 4 atom %, it is in the inclination for the magnetic properties of a rare earth magnet 100 to deteriorate.

[0046]

moreover, from a viewpoint of improvement in the coercive force of a rare earth magnet 100, the improvement in productivity, and low-cost-izing Aluminum (aluminum), titanium (Ti), vanadium (V), chromium (Cr), Manganese (Mn), a bismuth (Bi), niobium (Nb), a tantalum (Ta), Molybdenum (Mo), a tungsten (W), antimony (Sb), germanium (germanium), One or more sorts of elements of tin (Sn), a zirconium (Zr), nickel (nickel), silicon (Si), a gallium (Ga), copper (Cu), the hafniums (Hf), etc. may be added, and the magnet element assembly 10 may be constituted. In this case, when the addition of the above-mentioned element is made below into 10 atom % to the amount of all the atoms that constitute the magnet element assembly 10, it is desirable. When the addition of these elements exceeds 10 atom %, it is in the inclination for the magnetic properties of a rare earth magnet 100 to fall.

[0047]

In the magnet element assembly 10, oxygen (O), nitrogen (N), carbon (C), calcium (calcium), etc. may contain by within the limits below 3 atom % as an unescapable impurity to the amount of all the atoms that constitute the magnet element assembly 10. [0048]

The enlarged drawing of Ib part of the magnet element assembly 10 is shown in <u>drawing 1</u> (b). The magnet element assembly 10 contains the main crystal phase 50 which has the crystal structure of tetragonal system substantially, the grain boundary phase 70 which intervenes among these main crystal phases 50, and contains many rare earth elements, and the crystalline boron rich crystal phase 60 containing comparatively many boron formed in the grain boundary phase 70, and takes the structure of polycrystal. The particle size of the main crystal phase 50 which is a magnetic phase is desirable in it being about 1-100 micrometers. The boron rich crystal phase 60 and the grain boundary phase 70 are nonmagnetic phases. 0.5 volume %-50 volume % extent content of the these boron rich crystal phase 60 and the grain boundary phase 70 is usually carried out into the magnet element assembly 10. And the structure of such polycrystal is exposed to 10s of front faces of the magnet element assembly 10.

[0049]

Such a magnet element assembly 10 can be manufactured with a sintering process which is described below. First, the constituent of the request containing the element mentioned above is cast, and an ingot is obtained. Then, coarse grinding of the obtained ingot is carried out to the particle size of about 10-100 micrometers using a stamp mill etc., subsequently, it pulverizes in particle size of about 0.5-5 micrometers using a ball mill etc., and powder is obtained.

[0050]

Next, the obtained powder is preferably fabricated all over a magnetic field, and a Plastic solid is acquired. In this case, the magnetic field strength in a magnetic field is desirable in their being 10 or more kOes, and compacting pressure is desirable in it being about two 1 - 5 t/cm.

[0051]

Then, at 1000-1200 degrees C, the acquired Plastic solid is sintered for about 0.5 to 5 hours, and is quenched. In addition, a sintered atmosphere is desirable in their being inert gas ambient atmospheres, such as Ar gas. And the magnet element assembly 10 as shown in <u>drawing 1</u> (a) is preferably obtained in an inert gas ambient atmosphere by performing heat treatment (aging treatment) at 500-900 degrees C for 1 to 5 hours.

(Amorphous-izing)

Then, the surface of the magnet element assembly 10 is made amorphous, and the amorphous layer 20 shown in <u>drawing 2</u> and <u>drawing 3</u> is formed.

[0053]

Here, an amorphous substance is the structure where the atom has arranged irregularly and does not have, specific crystal structure, i.e., periodic array structure. It can judge easily whether the surface of a rare earth magnet 100 is amorphous, or it is polycrystal by whether electron diffraction and an X-ray diffraction method are performed, and the peak originating in a crystal lattice is observed intentionally. If amorphous, the peak originating in a crystal will not be observed. Moreover, it can judge by TEM observation etc. whether it is amorphous or it is polycrystal. [0054]

Specifically, the amorphous layer 20 can be formed by giving an impact to the surface of the magnet element assembly 10. As shown in <u>drawing 2</u>, by projecting the particle group 80 and making it collide to the surface of the magnet element assembly 10, the surface of the magnet element assembly 10 is made amorphous, it considers as the amorphous layer 20 and, more specifically, things can be carried out. When the so-called shot-peening method for projecting the spherical particle group 80 to the surface of the magnet element assembly 10 especially is adopted, wear of the surface in the case of amorphous-izing etc. does few and is desirable. In addition, even if it projects the abrasive grain which is a non-ball-like particle, surface amorphous-izing is possible. [0055]

As the quality of the material of the particle of the particle group 80, metals, such as a ceramic of SiO2, SiC, and aluminum2O3 grade and iron, are mentioned.
[0056]

The well-known blasting machine 71 as shown in <u>drawing 2</u> can perform projection of such a particle group 80 easily.

[0057]

This blasting machine 71 is equipped with the introductory pipe 76 of outlet 74b of the projection nozzle 74 introduced a little into a near side for the particle group 80 discharged from the lower limit of the projection nozzle 74, the pump 73 which supplies air to inlet-port 74a of this projection nozzle 74, the hopper 720 which stores the particle group 80, and a hopper 72. [0058]

Outlet 74b of the projection nozzle 74 is turned to the front face of the magnet element assembly 10, and if gas is supplied from a pump 73, the particle group 80 will be pulled out from a hopper 72 through the introductory pipe 76, and it will be projected on it toward the magnet element assembly 10 from outlet 74b of the projection nozzle 74. The particle group 80 on which it was projected hits the front face of the magnet element assembly 10. [0059]

Thus, although especially the temperature of the magnet element assembly 10 at the time of forming the amorphous layer 20 is not limited, its temperature at the time of membrane formation is desirable in it being extent which does not degrade the magnetic properties of the magnet element assembly 10. It is more desirable when it is desirable when temperature is maintained at 500 degrees C or less, and it maintains at 300 degrees C or less from such a viewpoint.

Thus, if an impact is given to the surface of the magnet element assembly 10 many times, according to this, very small plastic deformation will happen repeatedly in a surface. Therefore, according to the shear and compression operation in this case, atomic regular structure is confused and is considered that the amorphous layer 20 which makes amorphous and is shown in <u>drawing 2</u> and <u>drawing 3</u> forms. And when it is made amorphous by giving an impact, the comparatively precise amorphous layer 20 is formed and corrosion resistance will become still higher.

[0061]

And the rare earth magnet 100 as shown in <u>drawing 4</u> (a) and <u>drawing 4</u> (b) is obtained here by projecting the particle group 80 on all the surfaces of the magnet element assembly 10 so uniformly. [0062]

Thus, the rare earth magnet 100 concerning this manufactured operation gestalt is equipped with the wrap amorphous layer 20 for the whole front face of the magnet element assembly 10 and this magnet element assembly 10.

[0063]

Here, in the rare earth magnet 100 of this operation gestalt, when thickness of the amorphous layer 20 is set to 0.1-20 micrometers from the viewpoint of improvement in corrosion resistance, and a viewpoint of reservation of sufficient magnetic properties, it is desirable, and further when [from viewpoints such as a production cost,] 0.3-10 micrometers, it is more desirable. [0064]

Moreover, with the above-mentioned operation gestalt, you may have the field where polycrystal and an amorphous substance are intermingled in the boundary of the magnet element assembly 10 and the amorphous layer 20.

[0065]

According to this operation gestalt, the amorphous layer 20 is formed on the magnet element assembly 10. There is almost no atomic regular structure in the amorphous layer 20 of amorphous structure, and it is unordered structure. Therefore, the part (refer to <u>drawing 3</u>) which corrosion matter like the grain boundary phase 70 which intervenes between the main crystal phases 50 in the polycrystal structure of the magnet element assembly 10 tends to diffuse alternatively hardly exists in the amorphous layer 20. Therefore, it is hard to diffuse corrosion components, such as oxygen, inside the amorphous layer 20, and they fully function as a protective layer which protects the magnet element assembly 10 from corrosion components, such as oxygen. [0066]

Moreover, with this operation gestalt, since the surface of the magnet element assembly 10 is made amorphous and it is considering as the amorphous layer 20, this amorphous layer 20 contains all of the element R which constitutes the magnet element assembly 10, for example, rare earth elements, iron, and boron. Physical properties, such as coefficient of thermal expansion of the magnet element assembly 10 and the amorphous layer 20, become near by this. Therefore, the adhesion of the amorphous layer 20 and the magnet element assembly 10 becomes good, and it is fully controlled that a crack occurs in the amorphous layer 20, or the amorphous layer 20 separates from the magnet element assembly 10 in it etc.

[0067]

Moreover, since the surface of the magnet element assembly 10 is made amorphous by the collision of the particle group 80, a different element from the element which constitutes the magnet element assembly 10 hardly mixes to the amorphous layer 20. That is, in the magnet element assembly 10 and the amorphous layer 20, the presentation ratio of elements, such as the rare earth elements R which constitute the magnet element assembly 10, iron, and boron, becomes almost the same. Since the physical properties of the magnet element assembly 10 and the amorphous layer 20 will become very near if it becomes like this, it becomes [such adhesion] still higher and is desirable. [0068]

Moreover, when it does in this way and an amorphous layer stops being able to separate easily, generating of contamination components, such as particle from a rare earth magnet, decreases extremely, and is desirable.

[0069]

Here, detection and the quantum of the magnet element assembly 10 or the configuration element in the amorphous layer 20 can be checked using well-known presentation analysis methods, such as EPMA (X-ray microanalyser method), XPS (X-ray photoelectron spectroscopy) and AES (Auger electron spectroscopy), or EDS (energy dispersion mold X-ray fluorescent spectroscopy). Furthermore, presentation distribution of the component of above-mentioned each class can be grasped by analyzing the cross section which appears by cutting each class in the rare earth magnet 100 exposed using well-known technique, such as etching, or a rare earth magnet 100 using the above-mentioned presentation analysis method.

[0070]

Furthermore, with this operation gestalt, on the occasion of formation of the amorphous layer 20, since it is not necessary to heat the magnet element assembly 10, the magnet element assembly 10 cannot be put to an elevated temperature, but it can control that the magnetic properties of the magnet element assembly 10 deteriorate, and the high rare earth magnet 100 of magnetic properties can be offered.

[0071]

Such a rare earth magnet can be suitably used as the disk drive for the starter for a line printer and automobiles and a motor, a special motor, a servo motor, and magnetic recording media, a linear actuator, a voice coil motor, the motor for equipments, an industrial use motor, a loudspeaker, and a magnet for a nuclear-magnetic-resonance diagnosis.

[0072]

(The second operation gestalt)

Next, the manufacture approach of the rare earth magnet of the second operation gestalt and rare earth magnet 200 concerning this invention are explained, referring to drawing 5.

[0073]

The point that the manufacture approach of the rare earth magnet concerning a **** 2 operation gestalt and a rare earth magnet 200 differ from the manufacture approach of the first operation gestalt and a rare earth magnet 100 is a point in which the passivation layer 30 was formed on the amorphous layer 20, by carrying out chemical conversion of the surface of the amorphous layer 20 further.

[0074]

Here, chemical conversion is processing used as the passivation layer 30 whose corrosion resistance did the chemical operation to the surface of the amorphous layer 20, and improved rather than the original amorphous layer 20, and it differs from carrying out the laminating of other layers on the amorphous layer 20.

[0075]

As the chemical conversion approach, making a nitric acid, the oxygen plasma, and ozone contact, and making the precise oxide film as passivation film form is mentioned, for example to the surface of the amorphous layer 20. Moreover, contacting a phosphoric-acid zinc water solution and making the precise phosphate coat as passivation film form to the surface of the amorphous layer 20 is mentioned. Moreover, it can replace with a phosphoric-acid zinc water solution, and a passivation layer can be formed also by the chemical conversion using zirconium system processing liquid, manganese system processing liquid, molybdenum system processing liquid, etc. [0076]

The operation effectiveness by such passivation layer 30 is explained. Although it has corrosion resistance with the amorphous layer 20 sufficient also with the rare earth magnet 100 exposed to direct atmospheric air like the first operation gestalt, and there is amorphous layer 20 the very thing then gradually depending on the class of magnet element assembly 10 of a rare earth magnet 100, i.e., the constituent of the magnet element assembly 10, for example, the class and concentration of rare earth elements, it may corrode a little. And since the passivation layer 30 in this operation gestalt controls the corrosion of the amorphous layer 20, it raises the corrosion resistance of a rare earth magnet 200 further, and raises dependability further.

[0077]

Since adhesion with the amorphous layer 20 cannot exfoliate easily highly, corrosion resistance is fully maintained and, especially as for the passivation layer 30 which was formed of chemical conversion unlike carrying out the laminating (coating) of other layers, a life becomes long. [0078]

In the rare earth magnet 200 of this operation gestalt, the thickness of the passivation layer 30 is desirable in it being 0.1-20 micrometers from a viewpoint of improvement in corrosion resistance, and more desirable in the thickness of the passivation layer 30 being 1-5 micrometers from viewpoints, such as a production cost, further.

[0079]

Moreover, it is desirable in the thickness of viewpoints, such as reservation of sufficient magnetic properties, to the amorphous layer 20 being 0.1-20 micrometers, and more desirable in the thickness of the amorphous layer 20 being 0.3-10 micrometers from viewpoints, such as a production cost, further.

[0080]

As mentioned above, although the suitable operation gestalt of the rare earth magnet of this invention was explained, this invention is not limited to the above-mentioned operation gestalt. For example, the configuration of a manufacturing-with this operation gestalt rare earth magnet is not limited to a rectangular parallelepiped which was illustrated, but may have the configuration according to an application. Concretely, when used for the drive part or the motor for automobiles of a hard disk drive unit, you may be the pilaster which has the cross section of a circular intercept. Moreover, when used for an industrial use processing machine, you may be the shape of a ring, and a disc-like configuration.

[0081]

Moreover, the component of the magnet element assembly 10 is not restricted to the system containing rare earth elements R, iron, and boron, either, but the system containing one or more sorts

of rare earth elements and Co(es) or the system containing one or more sorts of rare earth elements, Fe(s), and nitrogen (N) is mentioned. The system which specifically contains Nd(s), such as a system containing Sm and Co(es), such as Sm-Co5 system or Sm2-Co17 system (a figure expresses an atomic ratio.), or a Nd-Fe-B system, and Fe and B is mentioned.

[0082]

Moreover, with the above-mentioned operation gestalt, although the amorphous layer 20 is formed all over the magnet element assembly 10, the amorphous layer 20 may be formed only in the part of a request of the front face of the magnet element assembly 10 if needed. Similarly, with the second operation gestalt, although the amorphous layer 20 is formed all over the magnet element assembly 10 and the passivation layer 30 is formed all over that amorphous layer 20, the part of a request of the front face of the magnet element assembly 10 may be covered with the amorphous layer 20, and a passivation layer may be further formed in the whole surface of this amorphous layer 20, or a desired part.

[0083]

Moreover, although an impact is given to the surface of the magnet element assembly 10 by the particle group 80 with the above-mentioned operation gestalt, the surface of the magnet element assembly 10 may be hit not with the particle group 80 but with a hammer etc. Moreover, the magnet element assembly 10 is put in with media, such as a particle, into a barrel, a barrel is rotated and the surface of the magnet element assembly 10 can be made amorphous also by giving an impact to the surface of the magnet element assembly 10 by the medium etc. moreover, instead of giving an impact to the surface of the magnet element assembly 10 -- the surface of the magnet element assembly 10 -- an atomic beam, a molecule beam, an ion beam, an electron ray, etc. -- irradiating -- etc. -- you may irradiate.

[0084]

In addition, although there is a case where the presentation ratio of the element with which an element moves to the amorphous layer 20, and constitutes the magnet element assembly 10 from the exterior in the magnet element assembly 10 and the amorphous layer 20 becomes less the same when the exposure of an atomic beam, a molecule beam, an ion beam, etc. performs amorphous-ization, a gap of a presentation ratio is sufficiently small even in this case, and the height of adhesion is demonstrated to some extent.

[0085]

Moreover, although chemical conversion of the surface of the amorphous layer 20 is carried out with the above-mentioned second operation gestalt, the laminating of resin, other metal layers, etc. may be carried out on the amorphous layer 20 without carrying out chemical conversion of the surface of the amorphous layer 20. even in this case, the conventional **** -- it is not necessary to form the precise film and can form by low cost using a simple approach.

[0086]

Moreover, in the above-mentioned rare earth magnet, it is also possible to form an amorphous layer by sputtering using the target containing the ingredient of the magnet element assembly 10 etc. [Example]

[0087]

Hereafter, although an example explains this invention to a detail further, this invention is not limited to these examples.

[0088]

(Example 1)

First, the sintered compact with the presentation of 14Nd-1Dy-7B-78Fe (a figure expresses an atomic ratio.) produced with powder-metallurgy processing of a rectangular parallelepiped was prepared as a magnet element assembly, the spherical particle group of SiO2 was projected to this magnet element assembly, and the whole surface surface was used as the amorphous layer. Spraying pressure of a particle was set to 0.4MPa(s) (about 4 kgf/cm2), and projected a total of a 0.5kg particle for 30 seconds here. Thus, the rare earth magnet of an example 1 was obtained. [0089]

When the cross section of the obtained rare earth magnet was observed by TEM, the thing with a surface contrastive with the polycrystal of a magnet element assembly been an amorphous

amorphous layer was checked. The thickness of this amorphous layer was 2 micrometers. [0090]

(Examples 2-4)

To the surface of the amorphous layer of the rare earth magnet obtained like the example 1, further, by performing chemical conversion, the passivation layer was formed and the rare earth magnet of examples 2-4 was obtained.

[0091]

In the example 2, it considered as H3PO4:12.5 g/L, ZnO;:1.3 g/L, NaNO3:3.0 g/L, and NaNo2:0.1 g/L, the amorphous layer of a rare earth magnet was immersed in the phosphoric-acid zinc water solution which adjusted pH to 2.8 by NaOH for 2 minutes at 65 degrees C, and chemical conversion was performed.

[0092]

In the example 3, the amorphous layer of a rare earth magnet was immersed in the nitric acid of 3% of concentration for 2 minutes, and chemical conversion was performed.

[0093]

In the example 4, the amorphous layer of a rare earth magnet was exposed to the pressure of 2Pa, and the oxygen plasma by RF (13.56MHz) excitation of injection power 250W for 5 minutes at the time of discharge, and chemical conversion was performed.

[0094]

(Example 1 of a comparison)

To the magnet element assembly without an amorphous layer, oxygen tension carried out scaling processing for 20 minutes with the heat treatment temperature of 600 degrees C in the argon atmosphere which is 1Torr, and made the surface of a magnet element assembly the low-grade oxide layer of the magnet element assembly ingredient as a protective layer.

[0095]

(Example 2 of a comparison)

To the front face of a magnet element assembly without an amorphous layer, the laminating of the protective layer made of an about 20-micrometer epoxy resin was carried out, and it considered as the protective layer.

[0096]

(Example 3 of a comparison)

To the surface of a magnet element assembly without an amorphous layer, with the phosphoric-acid zinc water solution of an example 2, chemical conversion was performed and the passivation layer was formed.

[0097]

In order to investigate corrosion resistance and magnetic properties, the following evaluation experiments were conducted on the rare earth magnet of examples 1-4 and the examples 1-3 of a comparison.

[0098]

About the obtained rare earth magnet, the humidification elevated-temperature trial (PCT trial) of 24 hours was performed in a steam ambient atmosphere, 120 degrees C, and two atmospheric pressures.

[0099]

About the rare earth magnet obtained in the examples 1-4, weight reduction before and after a PCT trial was not seen. Moreover, when the rare earth magnet after a PCT trial was observed visually, having not produced defects, such as a pinhole and a crack, was checked by the amorphous layer and passivation layer as a protective layer of a rare earth magnet. Furthermore, the flux loss before and after a PCT trial had stopped at 0.24% of measurement error range. Moreover, the residual magnetic flux density of the rare earth magnet after a PCT trial was 398 or more mTs.

On the other hand, about the rare earth magnet obtained in the examples 1-3 of a comparison, 0.3% or more of weight reduction was accepted. Moreover, when the rare earth magnet after a PCT trial was observed visually, it was observed that much fine particles have occurred on the front face. Moreover, flux losses before and after a PCT trial were 8.4% or more and a big value. Furthermore,

the residual magnetic flux density of the rare earth magnet after a PCT trial was 353 or less mTs. [Brief Description of the Drawings]

[0101]

[Drawing 1] The type section Fig. and <u>drawing 2</u> (b) which show the manufacture approach which <u>drawing 1</u> (a) requires for the 1st operation gestalt are the enlarged drawing of the surface Ib section of the magnet element assembly 10 of <u>drawing 1</u> (a).

[Drawing 2] Drawing 2 is a mimetic diagram following drawing 1 (a) which shows the manufacture approach of the 1st operation gestalt.

[Drawing 3] Drawing 3 is the expanded sectional view of the III section of drawing 2.

[Drawing 4] The perspective view and drawing 4 (b) which show the rare earth magnet which drawing 4 (a) requires for the 1st operation gestalt are the IVb-IVb view Fig. of drawing 4 (a). [Drawing 5] It is the outline sectional view showing the rare earth magnet of the 2nd operation gestalt of this invention.

[Drawing 6] It is the table showing the PTC test result of the rare earth magnet of examples 1-4 and the examples 1-3 of a comparison.

[Description of Notations]

[0102]

10 [-- A particle group, 100,200 / -- Rare earth magnet.] -- A magnet element assembly, 20 -- An amorphous layer, 30 -- A passivation layer, 80

[Translation done.]

* NOTICES *

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DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[0101]

[Drawing 1] The type section Fig. and drawing 2 (b) which show the manufacture approach which drawing 1 (a) requires for the 1st operation gestalt are the enlarged drawing of the surface Ib section of the magnet element assembly 10 of drawing 1 (a).

[Drawing 2] Drawing 2 is a mimetic diagram following drawing 1 (a) which shows the manufacture approach of the 1st operation gestalt.

[Drawing 3] Drawing 3 is the expanded sectional view of the III section of drawing 2.

[Drawing 4] The perspective view and <u>drawing 4</u> (b) which show the rare earth magnet which <u>drawing 4</u> (a) requires for the 1st operation gestalt are the IVb-IVb view Fig. of <u>drawing 4</u> (a).

[Drawing 5] It is the outline sectional view showing the rare earth magnet of the 2nd operation gestalt of this invention.

[Drawing 6] It is the table showing the PTC test result of the rare earth magnet of examples 1-4 and the examples 1-3 of a comparison.

[Translation done.]

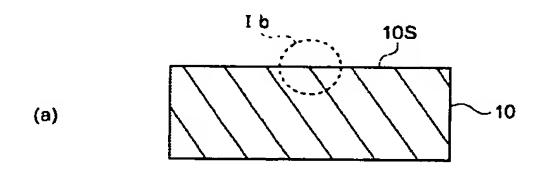
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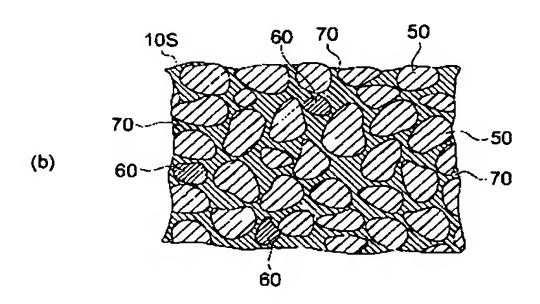
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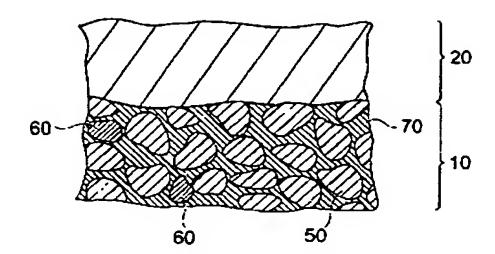
DRAWINGS

[Drawing 1]

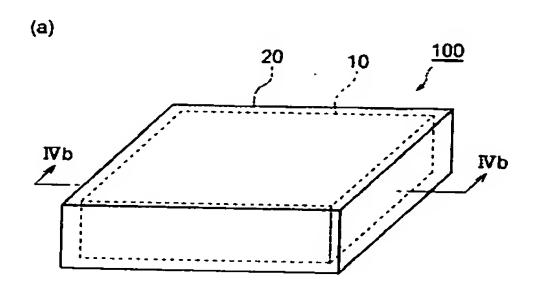


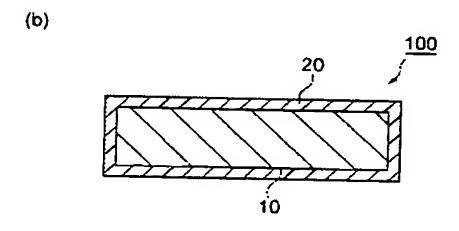


[Drawing 2]

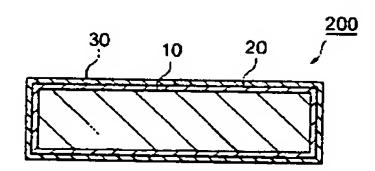


[Drawing 4]





[Drawing 5]



[Drawing 6]

	保護器の形成方法	PCTIAM	PCTILLE	界四田英
1		REMUN(10)	FILEX 1055 (%)	医 (集(mT)
英元第二	非品質化	0.04	新建物图	412
案施例2	养品贷化十七烷名语(5)7醇用给水溶液)	温克服等以下	は最初国	â
実施到3	非晶質化十化成処理(硝酸)	0.01	以表稿图	304
東施例4	非品質化+化成熟理(数集プラズマ)	湖定服界以下	は単の田	388
1.16क्ष	影処理による酸化	0.38	8.4	345
比较研2	樹脂を指揮	0.5B	10.5	353
比較例3	化成组现	0.41	9.1	348

[Translation done.]

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				中央区日本橋1丁目13番1号
		(74) 代理人		
			弁理士	長谷川 芳樹
		(74) 代理人		
			弁理士	寺崎 史朗
		(74) 代理人	1001082	
			弁理士	阿部 豊隆
		(74) 代理人	1001240	
			弁理士	三上 敬史
		(72) 発明者		
			東京都中	中央区日本橋一丁目13番1号 T
			DK株式	
				最終頁に続く

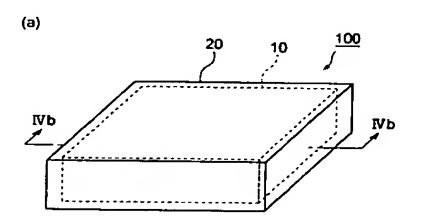
(54) 【発明の名称】希土類磁石の製造方法及び希土類磁石

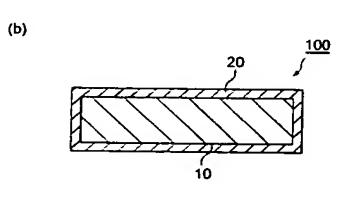
(57)【要約】

【課題】 十分に優れた磁気特性を有し、かつ、耐食性が十分に優れた希土類磁石の製造方法及び希土類磁石を提供する。

【解決手段】 本発明に係る希土類磁石の製造方法では、希土類元素を含みかつ多結晶質の磁石素体 10を用意し、この磁石素体 10の表層を非晶質化する非晶質化工程を備える。

【選択図】 図4





【特許請求の範囲】

【請求項1】

希土類元素を含みかつ多結晶質の磁石素体を用意し、前記磁石素体の表層を非晶質化す る非晶質化工程を備える希土類磁石の製造方法。

【請求項2】

前記非晶質化工程では、前記磁石素体の表層に衝撃を与えて前記磁石素体の表層を非晶 質化する請求項1に記載の希土類磁石の製造方法。

【請求項3】

前記非晶質化工程では、粒子群を前記磁石素体の表層に衝突させる請求項2に記載の希 土類磁石の製造方法。

【請求項4】

前記非晶質化工程では、前記磁石素体の表面から深さ 0.1~20μmまでの部分を非 晶質化する請求項1~3の何れかに記載の希土類磁石。

【請求項5】

前記非晶質化工程の後に、前記非晶質化された層の表層を化成処理して不動態化層を形 成する化成処理工程をさらに備える請求項1~4の何れかに記載の希土類磁石の製造方法

【請求項6】

前記化成処理工程では、前記非晶質層の表層に硝酸、燐酸亜鉛水溶液、酸素プラズマ、 及びオゾンの内少なくとも一つを接触させる請求項5に記載の希土類磁石の製造方法。

【請求項7】

希土類元素を含みかつ多結晶質の磁石素体と、

前記磁石素体上に形成された非晶質層と、を備え、

前記非晶質層は前記磁石素体を構成する元素を全て含む希土類磁石。

【請求項8】

前記磁石素体及び前記非晶質層において、前記磁石素体を構成する元素の組成比は同一 である請求項7に記載の希土類磁石。

【請求項9】

希土類元素を含みかつ多結晶質の磁石素体と、

前記磁石素体上に形成された非晶質層と、を備え、

前記非晶質層は前記磁石素体を非晶質化したものである希土類磁石。

【請求項10】

前記非晶質層は 0. 1~20 μmの厚みを有する請求項 7~9の何れかに記載の希土類 磁石。

【請求項11】

前記非晶質層上に、前記非晶質層を化成処理して不動態化した不動態化層をさらに備え る請求項7~10の何れか一項に記載の希土類磁石。

【発明の詳細な説明】

【技術分野】

[0001]

本発明は、希土類磁石の製造方法及び希土類磁石に関するものである。

【背景技術】

[0002]

従来より、高エネルギー積を示す永久磁石として、Nd等の希土類元素を含む希土類磁 石が知られている。この種の希土類磁石は、主成分として比較的容易に酸化される希土類 元素を含有するため、その耐食性が比較的低い。従って、これに起因して、製造時及び使 用時に磁石としての性能が劣化することや、製造された磁石の信頼性が比較的低いこと等 の課題があった。そして、このような希土類磁石の耐食性を改善することを目的として、 磁石素体の表面に保護層を形成する提案がなされている。

[0003]

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例えば特許文献1では、酸素分圧が10⁻⁶~1Torrであるアルゴン、窒素又は低真空雰囲気において、熱処理温度200~1100℃で10分~10時間の表面酸化処理を磁石素体に施し、磁石素体の表層を保護層としての磁石素体材料の低級酸化膜とする方法が提案されている。

[0004]

また、特許文献 2 には、磁石素体の表面に、 5 ~ 2 5 μ m程度の樹脂製の保護層を形成する方法が開示されている。

【特許文献1】特開2002-57052号公報

【特許文献2】特開昭60-63901号公報

【発明の開示】

【発明が解決しようとする課題】

[0005]

しかしながら、本発明者らが詳細に検討を行ったところ、従来の保護層を有する希土類 磁石には以下のような課題があることが判明した。

[0006]

すなわち、熱処理により磁石素体材料の表層を保護層としての酸化膜とした希土類磁石は、製造時に磁石素体が高温に曝されるために磁石素体における磁束等の磁気特性が劣化してしまう場合が多い。

[0007]

一方、樹脂等の保護層を磁石素体の表面に形成した希土類磁石は、磁石素体と保護層との間で熱膨張率等の物性の差が大きいため、保護層と磁石素体との密着性が十分でなく、保護層にクラックが生じたり保護層が剥がれやすくなったりする。このため、耐食性が不十分となる場合が多い。

[0008]

本発明は上記事情に鑑みてなされたものであり、十分に優れた磁気特性を有し、かつ、耐食性が十分に優れた希土類磁石の製造方法及び希土類磁石を提供することを目的とする。

【課題を解決するための手段】

[0009]

本発明に係る希土類磁石の製造方法は、希土類元素を含みかつ多結晶質の磁石素体を用意し、この磁石素体の表層を非晶質化する非晶質化工程を備える。

[0010]

ここで、多結晶質とは、原子が規則正しく配列した単結晶粒を多数集合してなる固体構造をいい、非晶質とは、原子が不規則に配列した固体構造をいう。

[0011]

一般に、希土類磁石は、希土類元素を含む結晶性の主相と、主相間に介在する希土類元素を含む粒界相と、を少なくとも含む多結晶質構造をとる。そして、粒界相には格子欠陥が多数含まれるため、この粒界相に対して酸素等の腐食成分が極めて拡散しやすい。また、希土類元素は元来酸素等の腐食成分によって腐食されやすい元素である。したがって、希土類磁石の表層に多結晶質の部分が露出していると、この粒界相に沿って腐食が進み、主相の結晶粒が脱落してしまう。

[0012]

ところが、本発明によれば、このような多結晶質の磁石素体の表層を非晶質化することにより、多結晶質の磁石素体上に、この磁石素体を覆う非晶質層を配した希土類磁石が形成される。この非晶質層には多結晶質のような原子の規則的な配列構造がほとんど無く、原子が不規則に配列している。従って、非晶質層には多結晶質における粒界相のように腐食物質が選択的に拡散しやすい部分が存在しにくく、この非晶質層には酸素等の腐食成分が拡散しにくい。これにより、この非晶質層は、多結晶質の磁石素体を酸素等の腐食成分から保護する保護層として機能する。

[0013]

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さらに、この非晶質層は、磁石素体を非晶質化したものであるため、磁石素体と非晶質層とは熱膨張率等の物性が互いに極めて近いものとなる。従って、非晶質層と磁石素体との密着性が良好となり、非晶質層にクラックが発生したり、非晶質層が磁石素体から剥がれたりし難くなる。これにより、希土類磁石は十分な耐食性を発揮することとなる。また、非晶質層のクラックの発生や剥がれが起こりにくいので、希土類磁石からのパーティクル等のコンタミ成分の発生が極めて少なくなり、好ましい。

[0014]

加えて、このような磁石素体の非晶質化は、磁石素体の表層に衝撃を与えることや、磁石素体の表層に原子ビーム、分子ビーム、イオンビーム、電子線等を照射すること等によって行えるので、磁石素体を高温にさらさずにすむ。したがって、製造時に磁石素体の磁束等の磁気特性がほとんど劣化せず、十分に優れた磁気特性を発揮しうる。

[0015]

ここで、非晶質化工程では、磁石素体の表層に衝撃を与えて磁石素体の表層を非晶質化することが好ましい。

[0016]

これによれば、容易に磁石素体の表層を非晶質化できる。また、原子ビーム、分子ビーム、イオンビーム、電子線等を照射して非晶質化するのに比して緻密な非晶質層を形成でき、非晶質層自体の腐食を十分に抑制できる。

[0017]

ここで、衝撃を与えることにより磁石素体が非晶質化する理由としては、例えば、機械的な衝撃を受けることにより磁石素体の表層に圧縮応力や剪断応力が加わって塑性変形が起こり、これによって、原子の規則的構造が乱れて非晶質化するものと考えられる。

[0018]

ここで、より具体的には、粒子群を磁石素体の表層に衝突させる、いわゆるブラスト、または、ショットピーニングといわれる方法を用いて磁石素体の表層に衝撃を与えることが好ましい。

[0019]

これによれば、磁石素体の表層に適度な衝撃を繰り返し与えることが容易である。特に、球状粒子群を用いると、磁石素体の表層の摩耗等を十分に抑制しつつ衝撃を与えられるので、きわめて効率よく非晶質化ができる。

[0020]

粒子の材料としては、例えば、 SiO_2 , SiC, AI_2O_3 等のセラミック材料が挙げられる。また、粒子の材料としてスチールショット等の金属材料を用いることもできる。

[0021]

また、非晶質化工程では、磁石素体の表面から深さ $0.1\sim20\mu$ mまでの部分を非晶質化すると好ましい。表面からの深さが 0.2μ m未満の部分のみを非晶質化しても、耐食性が十分発揮しにくくなる傾向がある。一方、表面からの 20μ m超の深さの部分までを非晶質化しても耐食性はそれ以上向上せず、非晶質化に要するコストが高くなって効率的でなくなる傾向がある。

[0022]

ところで、このようにして形成した非晶質層によって、希土類磁石の磁石素体を十分に保護することができるが、非晶質層の組成によっては非晶質層自体が若干腐食する場合がある。

[0023]

そこで、非晶質化工程の後に、非晶質層の表層を化成処理して不動態化層を形成する化成処理工程をさらに備えることが好ましい。

[0024]

この場合には、不動態化層によって非晶質層自体の腐食もさらに低減され、希土類磁石の耐食性のさらなる向上が可能となる。

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[0025]

化成処理として、具体的には、非晶質層の表層に硝酸、燐酸亜鉛水溶液、酸素プラズマ、及びオゾンの内少なくとも一つを接触させることが挙げられる。

[0026]

本発明の希土類磁石は、希土類元素を含みかつ多結晶質の磁石素体と、この磁石素体の表面を覆う非晶質層と、を備え、非晶質層は磁石素体を構成する元素を全て含む。

[0027]

本発明によれば、非晶質層には粒界相がほとんど存在せず、この非晶質層は、前述のように磁石素体を酸素等の腐食成分から保護する保護層として機能する。また、この非晶質層は、磁石素体の構成元素をすべて含んでいる。したがって、磁石素体と非晶質層との物性が互いに近いものとなり、非晶質層と磁石素体との密着性が良好となり、十分な耐食性を発揮する。

[0028]

また、このような構成の希土類磁石は、上述の製造方法によって磁石素体を高温にさらすことなく容易に製造することができる。したがって、磁気特性の十分に高い希土類磁石を実現できる。

[0029]

ここで、磁石素体及び非晶質層において、磁石素体を構成する元素の組成比は同一であることが好ましい。この場合には、非晶質層と磁石素体との物性がより近くなるので磁石素体と非晶質層との密着性をより向上できる。ここでは、例えば、磁石素体の表層に衝撃を与えることによりこのような非晶質層を形成できる。

[0030]

本発明に係る希土類磁石を別の観点から表現すると、本発明に係る希土類磁石は、希土類元素を含みかつ多結晶質の磁石素体と、磁石素体上に形成された非晶質層と、を備え、非晶質層はこの磁石素体を非晶質化したものである。

[0031]

このような希土類磁石は上述の希土類磁石と同様の作用効果を奏する。

[0032]

上述の何れの希土類磁石においても、非晶質層は $0.1\sim20\mu$ mの厚みを有することが好ましい。非晶質層の厚みが 0.1μ mよりも薄いと、耐食性を十分発揮しにくくなる傾向がある。一方、 20μ mよりも厚い非晶質層を形成しても耐食性はそれ以上向上せず、非晶質層の形成に要するコストが高くなって効率的でなくなる傾向がある。

[0033]

ここで、非晶質層上に、この非晶質層を化成処理してなる不動態化層をさらに有することが好ましい。この場合には、不動態化層によって、非晶質層自体の腐食もさらに低減されて希土類磁石の耐食性のさらなる向上が可能となる。

[0034]

このような希土類磁石における磁石素体としては、例えば、希土類元素、鉄、及び、ホウ素を含む磁石素体を用いることができる。この磁石素体は、磁気特性が極めて高いことで知られるが、本発明に係る希土類磁石にこの種の磁石素体を用いることによって、高い磁気特性を有しかつ高い耐食性を有する希土類磁石を得ることができる。

【発明の効果】

[0035]

本発明によれば、十分に優れた磁気特性及び耐食性を有する希土類磁石の製造方法及び希土類磁石を提供することができる。

【発明を実施するための最良の形態】

[0036]

以下、必要に応じて図面を参照しつつ、本発明の好適な実施形態について詳細に説明すた、上下左右等の位置関係は、特に断らない限り、図面に示す位置関係に基づくものとする。更に、図面の寸法比率は図示の比率に限られるものではない。

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[0037]

(第一実施形態)

まず本発明の第一実施形態に係る希土類磁石100の製造方法及び希土類磁石100について説明する。

[0038]

(磁石素体の用意)

まず、図1 (a)に示すように、希土類元素を含みかつ多結晶質の磁石素体10を用意する。

[0039]

破石素体10は、希土類元素R、鉄(Fe)及びホウ素(B)を含有する磁石である。 希土類元素Rは1種以上の希土類元素を示すものであり、具体的には、長周期型周期表の 3族に属するスカンジウム(Sc)、イットリウム(Y)及びランタノイドからなる群よ り選ばれる1種以上の元素を示す。ここで、ランタノイドは、ランタン(La)、セリウム(Ce)、プラセオジム(Pr)、ネオジム(Nd)、サマリウム(Sm)、ユウロピウム(Eu)、ガドリニウム(Gd)、テルビウム(Tb)、ジスプロシウム(Dy)、ホルミウム(Ho)、エルビウム(Er)、ツリウム(Tm)、イッテルビウム(Yb) 及びルテチウム(Lu)を指す。

[0040]

希土類元素 R としては、上述したもののうち、 N d 、 P r 、 H o 、 T b のうち 1 種以上の元素を含むと好ましく、さらに、 L a 、 S m 、 C e 、 G d 、 E r 、 E u 、 T m 、 Y b 、 Y のうち 1 種以上の元素を含んでも好ましい。

[0041]

磁石素体10中の希土類元素Rの含有割合は、磁石素体10を構成する全原子の量に対して、8~40原子%であると好ましい。希土類元素Rの含有割合が8原子%未満では、結晶構造がα一鉄と同一構造の立方晶組織となるため、高い保磁力(iHc)を有する希土類磁石100が得られない傾向にある。また、希土類元素Rの含有割合が40原子%を超えると、Rリッチな非磁性相が多くなり、希土類磁石100の残留磁束密度(Br)が低下する傾向にある。

[0042]

磁石素体10中のFeの含有割合は、磁石素体10を構成する全原子の量に対して、42~90原子%であると好ましい。Feの含有割合が42原子%未満であると希土類磁石100のBrが低下する傾向にあり、90原子%を超えると希土類磁石100のiHcが低下する傾向にある。

[0043]

磁石素体10中のBの含有割合は、磁石素体10を構成する全原子の量に対して、2~28原子%であると好ましい。Bの含有割合が2原子%未満であると結晶構造が菱面体組織となるため、希土類磁石100のiHcが不十分となる傾向にあり、28原子%を超えるとBリッチな非磁性相が多くなるため、希土類磁石100のBrが低下する傾向にある

[0044]

また、Feの一部をコバルト(Co)で置換して磁石素体10を構成してもよい。このような構成にすることにより、希土類磁石100の磁気特性を損なうことなく温度特性を改善できる傾向にある。この場合、置換後のFeとCoの含有割合は、原子基準でCo/(Fe+Co)が0.5以下であると好ましい。これよりもCoの置換量が多いと希土類磁石100の磁気特性が低下してしまう傾向にある。

[0045]

さらに、Bの一部を炭素(C)、リン(P)、硫黄(S)及び銅(Cu)からなる群より選ばれる1種以上の元素で置換して磁石素体10を構成してもよい。かかる構成にすることにより、希土類磁石100の生産性が向上し、その生産コストを削減できる傾向にある。この場合、これらC、P、S及び/若しくはCuの含有量は、磁石素体10を構成す

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る全原子の量に対して4原子%以下であると好ましい。C、P、S及び/若しくはCuの含有量が4原子%よりも多いと、希土類磁石100の磁気特性が劣化する傾向にある。

[0046]

また、希土類磁石100の保磁力の向上、生産性の向上及び低コスト化の観点から、アルミニウム(A 1)、チタン(T i)、バナジウム(V)、クロム(C r)、マンガン(M n)、ビスマス(B i)、ニオブ(N b)、タンタル(T a)、モリブデン(M o)、タングステン(W)、アンチモン(S b)、ゲルマニウム(G e)、スズ(S n)、ジルコニウム(Z r)、ニッケル(N i)、ケイ素(S i)、ガリウム(G a)、銅(C u)及び/又はハフニウム(H f)等のうちの1種以上の元素を添加して、磁石素体10を構成してもよい。この場合、上記元素の添加量は磁石素体10を構成する全原子の量に対してもよい。この場合、上記元素の添加量は磁石素体10を構成する全原子の量に対して10原子%以下とすると好ましい。これらの元素の添加量が10原子%を超えると希土類磁石100の磁気特性が低下する傾向にある。

[0047]

磁石素体10中には、不可避的不純物として、酸素(O)、窒素(N)、炭素(C)及び/又はカルシウム(Ca)等が、磁石素体10を構成する全原子の量に対して3原子%以下の範囲内で含有されていてもよい。

[0048]

磁石素体10のIb部分の拡大図を図1(b)に示す。磁石素体10は、実質的に正方晶系の結晶構造を有する主結晶相50と、これらの主結晶相50間に介在し希土類元素を多く含む粒界相70と、粒界相70内に形成されたホウ素を比較的多く含む結晶性のホウ素リッチ結晶相60と、を含有しており、多結晶質の構造をとる。磁性相である主結晶相50の粒径は1~100μm程度であると好ましい。ホウ素リッチ結晶相60及び粒界相70は、磁石素体10中に通常、0.5体積%~50体積%程度含有されている。そして、このような多結晶の構造が磁石素体10の表面10sに露出している。

[0049]

このような磁石素体 1 0 は、例えば以下に述べるような焼結法により製造できる。まず、前述した元素を含有する所望の組成物を鋳造し、インゴットを得る。続いて、得られたインゴットを、スタンプミル等を用いて粒径 1 0~1 0 0 μ m 程度に粗粉砕し、次いで、ボールミル等を用いて 0.5~5 μ m 程度の粒径に微粉砕して粉末を得る。

[0050]

次に、得られた粉末を、好ましくは磁場中にて成形して成形体を得る。この場合、磁場中の磁場強度は $1\ 0\ k\ O\ e\ 以上であると好ましく、成形圧力は <math>1\sim 5\ t\ /\ c\ m^2$ 程度であると好ましい。

[0051]

続いて、得られた成形体を1000~1200℃で0.5~5時間程度焼結し、急冷する。なお、焼結雰囲気は、Arガス等の不活性ガス雰囲気であると好ましい。そして、好ましくは不活性ガス雰囲気中で、500~900℃にて1~5時間熱処理(時効処理)を行うことにより、図1(a)に示すような、磁石素体10が得られる。

(非晶質化)

続いて、磁石素体10の表層を非晶質化して、図2及び図3に示す非晶質層20を形成する。

[0053]

ここで、非晶質とは、原子が不規則に配列しており特定の結晶構造、すなわち、周期的な配列構造を有さない構造である。希土類磁石100の表層が非晶質であるか多結晶質であるかは、例えば、電子線回折やX線回折法を行って、結晶格子に由来するピークが有意に観察されるか否かによって容易に判断できる。非晶質であれば結晶に由来するピークは観察されない。また、非晶質であるか多結晶質であるかは、TEM観察等によっても判断できる。

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[0054]

具体的には、磁石素体10の表層に衝撃を与えることにより非晶質層20を形成できる。より具体的には、図2に示すように、磁石素体10の表層に対して、粒子群80を投射して衝突させることにより磁石素体10の表層を非晶質化して非晶質層20とすることできる。特に、球状の粒子群80を磁石素体10の表層に対して投射する、いわゆるショットピーニング法を採用すると、非晶質化の際の表層の摩耗等も少なくできて好ましい。なお、非球状の粒子である砥粒等を投射しても表層の非晶質化は可能である。

[0055]

粒子群 8 0 の粒子の材質としては、 S i O $_2$ 、 S i C 、 A I $_2$ O $_3$ 等のセラミックや鉄等の金属が挙げられる。

[0056]

このような粒子群80の投射は、例えば、図2に示すような公知のブラスト装置71によって容易に行える。

[0057]

このブラスト装置 7 1 は、投射ノズル 7 4 と、この投射ノズル 7 4 の入口 7 4 a にエアを供給するポンプ 7 3 と、粒子群 8 0 を貯留するホッパ 7 2 0 と、ホッパ 7 2 の下端から排出される粒子群 8 0 を投射ノズル 7 4 の出口 7 4 b のやや手前側に導入する導入パイプ 7 6 と、を備えている。

[0058]

投射ノズル74の出口74bは磁石素体10の表面に向けられており、ポンプ73からガスが供給されると、粒子群80が導入パイプ76を介してホッパ72から引き出され、投射ノズル74の出口74bから磁石素体10に向かって投射される。投射された粒子群80は、磁石素体10の表面を打撃する。

[0059]

このようにして、非晶質層20を形成する際の磁石素体10の温度は特に限定されないが、成膜時の温度が磁石素体10の磁気特性を劣化させない程度であると好ましい。そのような観点から、温度を500℃以下に維持すると好ましく、300℃以下に維持するとより好ましい。

[0060]

このようにして、磁石素体10の表層に衝撃が多数回与えられると、これに応じて表層において微少な塑性変形が繰り返し起こる。したがって、この際の剪断や圧縮作用によって、原子の規則的構造が乱れて非晶質化し図2及び図3に示す非晶質層20が形成するものと考えられる。そして、衝撃を与えることにより非晶質化した場合は、比較的緻密な非晶質層20が形成され耐食性が一層高いものとなる。

[0061]

そして、ここでは、磁石素体10の全表層にたいしてまんべんなく粒子群80を投射することにより、図4(a)及び図4(b)に示すような希土類磁石100が得られる。

[0062]

このようにして製造した本実施形態に係る希土類磁石100は、磁石素体10と、この磁石素体10の表面全体を覆う非晶質層20と、を備えている。

[0063]

ここで、本実施形態の希土類磁石100においては、耐食性の向上の観点及び十分な磁気特性の確保の観点から、その非晶質層20の膜厚を0.1~20 μ mとすると好ましく、更に生産コスト等の観点から0.3~10 μ mとすると、より好ましい。

[0064]

また、上記実施形態では、磁石素体10と非晶質層20との境界には、多結晶質と非晶質とが混在する領域を有していてもよい。

[0065]

本実施形態によれば、磁石素体10の上に非晶質層20が形成されている。非晶質構造の非晶質層20には、原子の規則的な構造がほとんど無く不規則構造である。従って、非

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品質層20には、磁石素体10の多結晶質構造において主結晶相50間に介在する粒界相70のような、腐食物質が選択的に拡散しやすい部分(図3参照)がほとんど存在しない。従って、酸素等の腐食成分が非晶質層20の内部に拡散し難く、磁石素体10を酸素等の腐食成分から保護する保護層として十分に機能する。

[0066]

また、本実施形態では、磁石素体10の表層を非晶質化して非晶質層20としているので、この非晶質層20は、磁石素体10を構成する元素、例えば、希土類元素 R、鉄、ホウ素を全て含む。これによって磁石素体10と非晶質層20との熱膨張率等の物性が近くなる。したがって、非晶質層20と磁石素体10との密着性が良好となり、非晶質層20にクラックが発生したり、非晶質層20が磁石素体10から剥がれたりすること等が十分に抑制される。

[0067]

また、粒子群80の衝突によって磁石素体10の表層を非晶質化しているので、非晶質層20に対して、磁石素体10を構成する元素とは異なる元素がほとんど混入しない。すなわち、磁石素体10及び非晶質層20とにおいて、磁石素体10を構成する希土類元素R、鉄、ホウ素等の元素の組成比はほぼ同一となる。こうなると磁石素体10と非晶質層20との物性が極めて近くなるのでこれらの密着性が一層高くなって好ましい。

[0068]

また、このようにして、非晶質層が剥がれにくくなると、希土類磁石からのパーティクル等のコンタミ成分の発生が極めて少なくなり好ましい。

[0069]

ここで、磁石素体10や非晶質層20中の構成元素の検出及び定量はEPMA(X線マイクロアナライザー法)、XPS(X線光電子分光法)、AES(オージェ電子分光法)若しくはEDS(エネルギー分散型蛍光 X線分光法)等の公知の組成分析法を用いて確認することができる。さらに、エッチング等の公知の手法を用いて露出させた希土類磁石100中の各層を、あるいは、希土類磁石100を切断することにより現れる断面を、上記の組成分析法を用いて分析することにより、上述の各層の構成材料の組成分布を把握することができる。

[0070]

さらに、本実施形態では、非晶質層20の形成に際し、磁石素体10を加熱しなくてよいので磁石素体10が高温に曝されず、磁石素体10の磁気特性が劣化することを抑制でき、磁気特性の高い希土類磁石100を提供できる。

[0071]

このような希土類磁石は、ラインプリンター、自動車用スターター及びモーター、特殊モーター、サーボモーター、磁気記録装置用ディスク駆動、リニアアクチュエーター、ボイスコイルモーター、装置用モーター、工業用モーター、スピーカー及び核磁気共鳴診断用の磁石として好適に使用することができる。

[0072]

(第二実施形態)

次に、本発明に係る第二実施形態の希土類磁石の製造方法及び希土類磁石200について、図5を参照しながら説明する。

[0073]

本第二実施形態に係る希土類磁石の製造方法及び希土類磁石200が第一実施形態の製造方法及び希土類磁石100と異なる点は、さらに非晶質層20の表層を化成処理することによって非晶質層20上に不動態化層30を形成した点である。

[0074]

ここで、化成処理とは、非晶質層 2 0 の表層に対して化学的な作用を及ぼして元の非晶質層 2 0 よりも耐食性が向上した不動態化層 3 0 にさせる処理であり、非晶質層 2 0 上に他の層を積層するのとは異なる。

[0075]

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化成処理方法としては、例えば、非晶質層 2 0 の表層に対して、硝酸、酸素プラズマ、オゾンに接触させて不動態化膜としての緻密な酸化膜を形成させることが挙げられる。また、非晶質層 2 0 の表層に対して、リン酸亜鉛水溶液を接触させて不動態化膜としての緻密なリン酸塩皮膜を形成させることが挙げられる。また、リン酸亜鉛水溶液に代えて、ジルコニウム系処理液、マンガン系処理液、モリブデン系処理液等を用いた化成処理によっても不動態化層を形成することができる。

[0076]

このような不動態化層30による作用効果について説明する。第一実施形態の如く非晶質層20が直接大気に露出する希土類磁石100でも十分な耐食性を有するが、希土類磁石100の磁石素体10の種類、すなわち、磁石素体10の構成成分、たとえば、希土類元素の種類や濃度によっては非晶質層20自体が徐々にではあるが若干腐食する場合がある。そして、本実施形態における不動態化層30は、非晶質層20の腐食を抑制するので、希土類磁石200の耐食性をさらに向上させ、信頼性を一層向上させる。

[0077]

特に、他の層を積層(コーティング)するのとは異なり、化成処理により形成された不動態化層30は、非晶質層20との密着性が高く剥離しにくいので、耐食性が十分に維持されて寿命が長くなる。

[0078]

本実施形態の希土類磁石 2 0 0 においては、不動態化層 3 0 の膜厚は、耐食性の向上の観点から、 0 . 1 ~ 2 0 μ mであると好ましく、更に生産コスト等の観点から不動態化層 3 0 の膜厚が 1 ~ 5 μ mであるとより好ましい。

[0079]

また、十分な磁気特性の確保等の観点から、非晶質層 2 0 の膜厚が 0 . 1 ~ 2 0 μ m であると好ましく、更に生産コスト等の観点から非晶質層 2 0 の膜厚が 0 . 3 ~ 1 0 μ m であるとより好ましい。

[0080]

以上、本発明の希土類磁石の好適な実施形態について説明したが、本発明は上記実施形態に限定されるものではない。例えば、本実施形態で製造するの希土類磁石の形状は、図示したような直方体に限定されず、用途に応じた形状を有していてよい。具体的に、ハードディスク装置の駆動部分若しくは自動車用モーターに用いられる場合は、円弧状切片の断面を有する柱形であってもよい。また、工業用加工機械に用いられる場合は、リング状や円板状の形状であってもよい。

[0081]

また、磁石素体 100 の構成材料も、希土類元素 R、鉄、ホウ素を含有する系に限られず、 1 種以上の希土類元素とCo とを含有する系、あるいは 1 種以上の希土類元素とFe と窒素 (N) とを含有する系などが挙げられる。具体的には、例えば、 $Sm-Co_5$ 系若しくは Sm_2-Co_{1-7} 系(数字は原子比を表す。)などのSm とCo とを含有する系、あるいは、Nd-Fe-B 系などのNd とFe とB とを含む系などが挙げられる。

[0082]

また、上記実施形態では、磁石素体10の全面に非晶質層20を形成しているが、必要に応じて磁石素体10の表面の所望の部分のみに非晶質層20を形成しても良い。同様に第二実施形態では、磁石素体10の全面に非晶質層20を形成し、その非晶質層20の全面に不動態化層30を形成しているが、磁石素体10の表面の所望の部分を非晶質層20で被覆し、さらに、この非晶質層20の全面又は所望の部分に不動態化層を形成してもよい。

[0083]

また、上記実施形態では粒子群80により磁石素体10の表層に衝撃を与えているが、粒子群80でなくハンマー等によって磁石素体10の表層を打撃してもよい。また、バレル中に粒子等の媒体と共に磁石素体10を入れ、バレルを回転させて媒体によって磁石素体10の表層に衝撃を与える等の方法でも磁石素体10の表層を非晶質化し得る。また、

磁石素体10の表層に衝撃を与える代わりに、磁石素体10の表層に、原子ピーム、分子ビーム、イオンビーム、電子線等を照射して等を照射してもよい。

[0084]

なお、原子ビーム、分子ビーム、イオンビーム等の照射により非晶質化を行った場合等には元素が外部から非晶質層 2 0 に移動し、磁石素体 1 0 と非晶質層 2 0 とにおいて、磁石素体 1 0 を構成する元素の組成比が同一でなくなる場合があるが、この場合でも組成比のずれは十分小さいものであり密着性の高さはある程度発揮される。

[0085]

また、上記第二実施形態では非晶質層 2 0 の表層を化成処理しているが、非晶質層 2 0 の表層を化成処理しないで、非晶質層 2 0 上に、樹脂や他の金属層等を積層してもよい。この場合でも、従来の如き緻密な膜を形成する必要はなく、簡便な方法を用いて低コストで形成可能である。

[0086]

また、上記希土類磁石においては、非晶質層を、例えば、磁石素体10の材料等を含むターゲットを用いたスパッタリング等によって形成することも可能である。

【実施例】

[0087]

以下、実施例により本発明を更に詳細に説明するが、本発明はこれらの実施例に限定されるものではない。

[0088]

(実施例1)

まず、粉末冶金法によって作製した 14Nd-1Dy-7B-78Fe (数字は原子比を表す。)の組成をもつ直方体の焼結体を磁石素体として用意し、この磁石素体に対して SiO_2 の球状粒子群を投射し、表層全面を非晶質層とした。ここで粒子の吹付圧力は 0 . 4MPa (約 4kg f / c m 2)とし、 30 秒間、合計 0 . 5kg の粒子を投射した。 このようにして実施例 1 の希土類磁石を得た。

[0089]

得られた希土類磁石の断面をTEMで観察したところ、表層は、磁石素体の多結晶質とは対照的な、非晶質の非晶質層となっていることが確認された。この非晶質層の厚みは 2 μ mであった。

[0090]

(実施例2~4)

実施例1と同様にして得た希土類磁石の非晶質層の表層に対して、さらに、化成処理を行うことにより不動態化層を形成し、実施例2~4の希土類磁石を得た。

[0091]

実施例2では、 H_3 PO $_4$: 12.5g/L、ZnO;:1.3g/L、NaNO $_3$: 3.0g/L、NaNo $_2$:0.1g/Lとし、pHをNaOHで2.8に調整したリン酸亜鉛水溶液に希土類磁石の非晶質層を65℃で2分間浸漬して化成処理を行った。

[0092]

実施例3では、濃度3%の硝酸に希土類磁石の非晶質層を2分間浸漬して化成処理を行った。

[0093]

実施例4では、放電時圧力2Pa、投入電力250Wの高周波(13.56MHz)励起による酸素プラズマに希土類磁石の非晶質層を5分間暴露して化成処理を行った。

[0094]

(比較例1)

非晶質層のない磁石素体に対して、酸素分圧が1Torrであるアルゴン雰囲気において熱処理温度600℃で20分間表面酸化処理し、磁石素体の表層を保護層としての磁石素体材料の低級酸化物層とした。

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(比較例2)

非晶質層のない磁石素体の表面に対して、20μm程度のエポキシ樹脂製の保護層を積 層して保護層とした。

[0096]

(比較例3)

非晶質層のない磁石素体の表層に対して、実施例2のリン酸亜鉛水溶液によって化成処理を施して不動態化層を形成した。

[0097]

耐食性及び磁気特性を調べるために、実施例1~4、比較例1~3の希土類磁石に以下のような評価実験を行った。

[0098]

得られた希土類磁石について、水蒸気雰囲気、120℃、2気圧において24時間の加湿高温試験(PCT試験)を行った。

[0099]

実施例1~4で得られた希土類磁石については、PCT試験前後での重量減少は見られなかった。また、PCT試験後の希土類磁石を目視で観察したところ、希土類磁石の保護層としての非晶質層や不動態化層にピンホール、クラック等の欠陥は生じていないことが確認された。さらに、PCT試験前後でのフラックスロスは0.24%の測定誤差範囲に止まっていた。また、PCT試験後)の希土類磁石の残留磁束密度は398mT以上であった。

[0100]

一方、比較例 1 ~ 3 で得られた希土類磁石については、 0 . 3 %以上の重量減少が認められた。また、 P C T 試験後の希土類磁石を目視で観察したところ、表面に粉体が多数発生しているのが観測された。また、 P C T 試験前後でのフラックスロスは 8 . 4 %以上と大きな値であった。さらに、 P C T 試験後の希土類磁石の残留磁束密度は 3 5 3 m T 以下であった。

【図面の簡単な説明】

[0101]

【図1】図1(a)は、第1の実施形態に係る製造方法を示す模式断面図、図2(b)は図1(a)の磁石素体10の表層Ib部の拡大図である。

【図2】図2は、第1の実施形態の製造方法を示す図1(a)に続く模式図である。

【図3】図3は、図2のIII部の拡大断面図である。

【図4】図4(a)は、第1の実施形態に係る希土類磁石を示す斜視図、図4(b)は、図4(a)のIVb-IVb矢視図である。

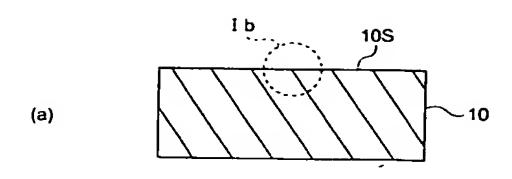
【図5】本発明の第2の実施形態の希土類磁石を示す概略断面図である。

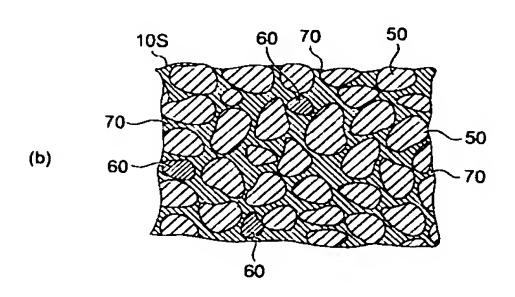
【図6】実施例1~4及び比較例1~3の希土類磁石のPTC試験結果を示す表である。 【符号の説明】

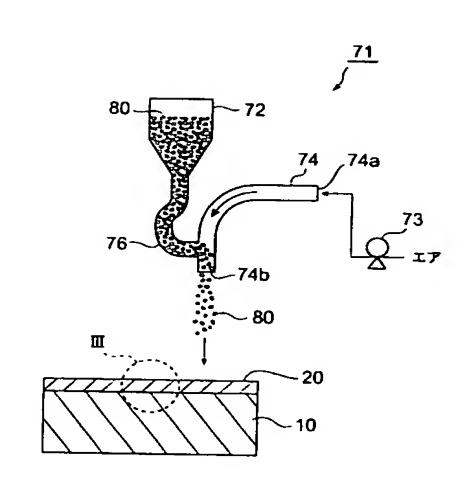
[0102]

10…磁石素体、20…非晶質層、30…不動態化層、80…粒子群、100,200…希土類磁石。

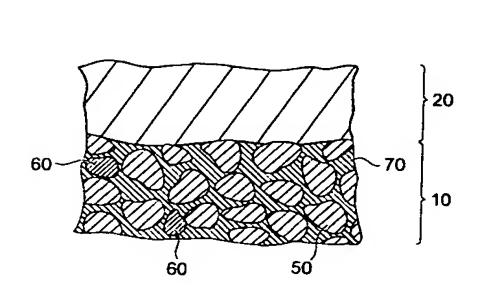
[図2]



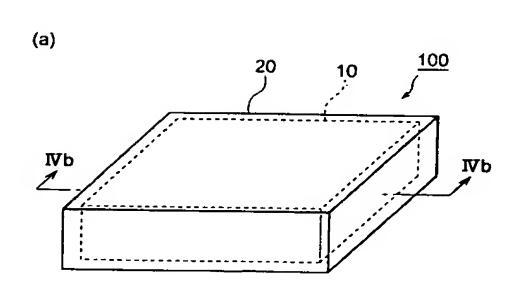


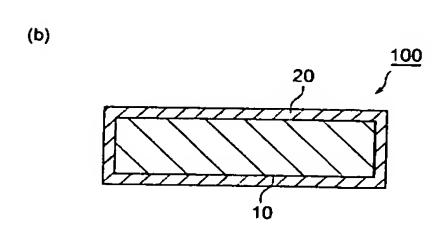


【図3】

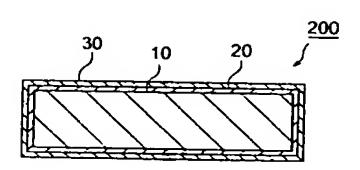


【図4】





【図6】



	保護層の形成方法	PCTば 第五 章少(%)	PCTIMIN Flux loss (%)	務留組束 医底(mT)
製品金1	北西京	0.04	四年四日	412
策略倒2	非品質化十化成処理(リン酸亜鉛水溶液)	剩定歷界以下	以整构图	405
東部第3	非晶質化十化成処理(硝酸)	0.01	はない国	88
家店倒4	非品質化+化成処理(酸素プラズマ)	到定限界以下	は神神田田	388
比较例1	熱処理による酸化	0.36	8.4	345
比較例2	併悶を積層	0.58	10.5	353
比較例3	化成构理	0.41	9.1	37.8

フロントページの続き

(72)発明者 田中 美知 東京都中央区日本橋一丁目 1 3 番 1 号 T D K 株式会社内

(72)発明者 坂本 健 東京都中央区日本橋一丁目13番1号 TDK株式会社内

(72)発明者 三輪 将史

東京都中央区日本橋一丁目13番1号 TDK株式会社内

F ターム(参考) 4K018 AA27 BA18 CA04 CA11 DA11 DA31 FA08 KA45 5E062 CD06 CG01 CG07

INTERNATIONAL SEARCH REPORT

International application No.

			PCT/JP200	
A. CLASSIFI Int.Cl	ICATION OF SUBJECT MATTER 100 H01F41/02, C22C38/00		101/0220	5/005//0
According to In	nternational Patent Classification (IPC) or to both natio	nal classification and IPC		
B. FIELDS SI	EARCHED			
Minimum docu Int . Cl	mentation searched (classification system followed by end of H01F41/02, C22C38/00	classification symbols)		
Kokai J	itsuyo Shinan Koho 1971-2005 T	Jitsuyo Shinan Toro Oroku Jitsuyo Shir	oku Koho 199 nan Koho 199	96-2005 94-2005
	base consulted during the international search (name of NTS CONSIDERED TO BE RELEVANT	l'data base and, where pract	icable, search terms u	ised)
Category*	Citation of document, with indication, where a			
X Y	JP 2004-002911 A (Yaskawa E) 08 January, 2004 (08.01.04), Claims; Par. Nos. [0004], [0 (Family: none)	_	0 3	1,2,4-6,8, 0-12,18-20, 24,25,28 ,7,9,13-17, 1-23,26,27, 29,30
Y	JP 03-115522 A (Seiko Instru 16 May, 1991 (16.05.91), Claims; page 1, lower right of 16 to page 2, upper right col page 2, lower left column; to (Family: none)	column, line lumn, line 1;	3	,2,5,6,8,9, 18-21,28 ,4,7,10-17, 22-27,29,30
× Further doc	cuments are listed in the continuation of Box C.	See patent family a	onnex.	
	gories of cited documents:	"I" later document publish	ed after the internation	al filing date or priority
"A" document de to be of partici "E" earlier applica filing date	efining the general state of the art which is not considered cular relevance ation or patent but published on or after the international	the principle or theory in "X" document of particular	ed after the internation with the application buunderlying the invention relevance; the claimed annot be considered to	if cited to understand n Linvention appear to
special reasor "O" document refe "P" document put the priority de		"Y" document of particular considered to involve	of is taken alone relevance; the claimed is an inventive step who more other such documes on skilled in the art	invention cannot be
Date of the actual 24 June	completion of the international search, 2005 (24.06.05)	Date of mailing of the inte 12 July, 20	ernational search repo 05 (12.07.05	ort 5)
	e Patent Office	Authorized officer		

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Y	JP 2003-007556 A (Nippon Kabaraijingu Kabushiki Kaisha), 10 January, 2003 (10.01.03), Claims; Par. No. [0020] (Family: none)	3,13,22,23
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